# APPENDIX A3.2 <br> FLOW COMPUTATION METHODS USED TO CALCULATE EAA BASIN FLOWS 

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## GATED SPILLWAYS

## Parameters

$\mathrm{C}_{\mathrm{cf}}=$ discharge coefficient for controlled free flow
Ccs = discharge coefficient for controlled submerged flow
Cot = discharge coefficient for over-the-top flow
Cuf = discharge coefficient for uncontrolled free flow
Cus = discharge coefficient for uncontrolled submerged flow
Go = gate opening, in feet
g $\quad=\quad$ acceleration due to gravity, $32.2 \mathrm{ft} / \mathrm{sec}^{2}$
$\mathrm{H}=$ approach head over the spillway sill, which is the difference between the upstream stage and the sill elevation, in feet
$\mathrm{Hg}_{\mathrm{g}} \quad=\quad$ approach head over the gate, in feet
$\mathrm{h}=$ submergence head over the spillway sill, which is the difference between the downstream stage and the sill elevation, in feet
$\mathrm{L} \quad=\quad$ length of spillway sill perpendicular to flow, in feet
$\mathrm{n}_{1} \quad=\quad$ exponent of approach head
$\mathrm{n}_{2} \quad=\quad$ exponent of submergence head
$\mathrm{n}_{3}=\quad$ exponent of total head
$\mathrm{n}_{4} \quad=\quad$ exponent of gate opening
$\mathrm{W} \quad=\quad$ width of gate, in feet

Uncontrolled Free Flow
$Q=C_{u f} L H^{n_{1}}$

| Spillway |
| :---: |
| S-5AS |
| S-7 |
| S-8 |
| S-351 |
| S-352 |
| S-354 |
| G-371 |
| G-373 |

Uncontrolled Submerged Flow

$$
Q=C_{u s} L h^{n_{2}}(H-h)^{n_{3}} \sqrt{2 g}
$$

| Spillway |
| :---: |
| S-5AS |
| S-7 |
| S-8 |
| S-351 |
| S-352 |
| S-354 |
| G-371 |
| G-373 |

Controlled Free Flow
$Q=C_{c f} L G_{o} \sqrt{2 g\left(H-0.5 G_{o}\right)}$

| Spillway |
| :---: |
| S-5AS |
| S-7 |
| S-8 |
| S-351 |
| S-352 |
| S-354 |
| G-371 |
| G-373 |

Controlled Submerged Flow
$Q=C_{c s} L G_{o}^{n_{4}} h^{n_{2}} \sqrt{2 g(H-h)}$

| Spillway |
| :---: |
| S-5AS |
| S-7 |
| S-8 |
| S-351 |
| S-352 |
| S-354 |
| G-371 |
| G-373 |

Over-the-top Flow

$$
Q=C_{o t} W H_{g}^{1.5} \sqrt{2 g}
$$

| Spillway |
| :---: |
| S-5AS |
| S-7 |
| S-8 |
| S-351 |
| S-352 |
| S-354 |

## PUMPS

## Parameters

| C | $=$ | coefficient of discharge for siphon |
| :---: | :---: | :---: |
| $\mathrm{C}_{0}-\mathrm{C}_{9}$ | $=$ | coefficients of pump rating equation |
| H | = | head, downstream stage minus upstream stage, in feet |
| Hfact | = | normalizing head factor, in feet |
| $\mathrm{H}_{\mathrm{hi}}$ | = | head from affinity laws corresponding to the high rpm rating equation, in feet |
| Hıo | $=$ | head from affinity laws corresponding to the low rpm rating equation, in feet |
| N | $=$ | engine speed, in rpm |
| $\mathrm{N}_{\text {fact }}$ | = | normalizing engine speed factor, in rpm |
| $\mathrm{N}_{\text {hi }}$ | = | engine speed of high rating equation, in rpm |
| $\mathrm{N}_{\text {lo }}$ | $=$ | engine speed of low rating equation, in rpm |
| $\mathrm{N}_{\text {min }}$ | = | minimum engine speed below which no discharge is possible, in rpm |
| n | = | exponent of head for siphon |
| X | = | normalized head parameter |
| Y | = | normalized engine speed parameter |

## Pump Flow

Constant-speed Pump
A single-variable polynomial is used.

$$
Q=C_{0}+C_{1} H+C_{2} H^{2}+C_{3} H^{3}
$$

| Pump |
| :---: |
| G-200A |
| G-200B |
| G-349B |
| G-350B |

## Variable-speed Pump

Interpolation of single-variable polynomials is performed. The pump affinity laws are used to obtain the adjusted head, $\mathrm{H}_{\mathrm{lo}}$ :
$H_{l o}=H\left(\frac{N_{l o}}{N}\right)^{2}$
The adjusted head $\mathrm{H}_{\mathrm{lo}}$ is used to compute Qlo.
$Q_{l o}=C_{0}+C_{1} H_{l o}+C_{2} H_{l o}^{2}+C_{3} H_{l o}^{3}$

| Pump |
| :---: |
| S-5A |
| S-6 |
| S-7 |
| S-8 |
| G-404 |
| G-410 |
| EBPS |
| ESPS |
| G-507 |
| G-370 |
| G-372 |
| SSDD |
| SFCD |
| G-434 |
| G-435 |
| C-10 |
| C-12A |
| C-12 |
| C-4A |
| S236 |
| EPD07 |

The adjusted head, $\mathrm{H}_{\mathrm{hi}}$ is:

$$
H_{h i}=H\left(\frac{N_{h i}}{N}\right)^{2}
$$

The adjusted head $\mathrm{H}_{\mathrm{hi}}$ is used to compute $\mathrm{Q}_{\mathrm{h}}$.

$$
Q_{h i}=C_{0}+C_{1} H_{h i}+C_{2} H_{h i}^{2}+C_{3} H_{h i}^{3}
$$

The affinity laws are used to obtain the discharge Q at engine speed N :
$Q=Q_{l o}+\left(Q_{h i}-Q_{l o}\right)\left(\frac{N-N_{l o}}{N_{h i}-N_{l o}}\right)$
Variable-speed Pump with Very Variable Head
A two-variable polynomial used. The normalized head and engine speed are:
$X=\frac{H}{H_{\text {fact }}}$
$Y=\frac{N-N_{\text {min }}}{N_{\text {fact }}}$

| Pump |
| :---: |
| S-2 |
| S-3 |

The pump discharge is:

$$
Q=C_{0}+C_{1} X+C_{2} Y+C_{3} X^{2}+C_{4} X Y+C_{5} Y^{2}+C_{6} X^{3}+C_{7} Y X^{2}+C_{8} X Y^{2}+C_{9} Y^{3}
$$

Siphon Flow
The siphon discharge is:
$Q=C H^{n}$

| Siphon |
| :---: |
| S-6 |

## CULVERTS

Refer to:

Fan, A. (October 1985). A General Program to Compute Flow through Gated Culverts (Technical Memorandum). West Palm Beach: South Florida Water Management District, West Palm Beach.

## Parameters

The parameter defined here correspond to the variables defined by A. Fan.

| Barrel $=$ | barrel shaped coding, "0" = circular, " 1 " = box |
| :---: | :---: |
| C | orifice flow coefficient due to inlet shape |
| Cw | weir flow coefficient (flashboard) |
| D | diameter of pipe culvert or height of box culvert, in feet |
| Gh | height of gate, in feet |
| Gtype | gate type coding, " 0 " = circular, " 1 " = rectangular, " 2 " = weir |
| Gw | width of gate, in feet |
| $\mathrm{IN}_{\mathrm{el}}$ | inlet invert elevation, in feet m.s.l. or NGVD |
| K | entrance loss coefficient due to shape of gate edge |
| L | length of culvert, in feet |
| N | number of barrels |
| n = | Manning's roughness coefficient |
| $\mathrm{OUT}_{\text {el }}=$ | outlet invert elevation, in feet m.s.l or NGVD |
| r = | refernece elevation for flashboard elevation, in feet m.s.l. or NGVD |
| $\mathrm{S}_{\mathrm{wb}}$ | total side weir length (riser or wing wall), in feet |
| $\mathrm{S}_{\text {we }}$ | side weir crest elevation (riser or wing wall), in feet |
| W | width of box culvert |
| $\mathrm{W}_{\mathrm{b}}$ | weir length (flashboad) |


| Culverts | Culverts |
| :---: | :---: |
| G-136 | G-402A |
| G-88 | G-402B |
| S-150 | G-402C |
| S-5AE | G-402D |
| G-357 | G-204 |
| G-205 | G-206 |
| G-376A | G-376D |
| G-379A | G-379D |
| G-381A | G-381C |
| G-722 |  |

